# Lecture 7. LMI approaches to $H_2$ , $H_\infty$ problems

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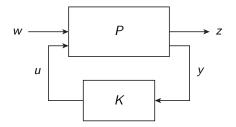
CDS270-2: Mathematical Methods in Control and System Engineering

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# Logistics

- hw6 due this Wed, May 13
  - do an easy problem or CYOA
  - use catalog with date stamp  $\geq 05/06/2015$
  - part 3(d): uses Matlab and CVX
- hw5 solutions posted online
- reading: Imibook Ch 4-6

## **Control system**



for a plant P and controller K we define the following signals

- exogenous inputs:  $w \in \mathbf{R}^{n_w}$
- actuator inputs:  $u \in \mathbf{R}^{n_u}$
- regulated outputs:  $z \in \mathbf{R}^{n_z}$
- sensed outputs:  $y \in \mathbf{R}^{n_y}$

## **Common signal measures**

Let  $y:[0,\infty) \to \mathbf{R}^n$  be a signal

 $L_\infty$  (peak) norm:

$$\|y\|_{\infty} = \max_{1 \le i \le n} \|y_i\|_{\infty} = \sup_{t > 0} \max_{1 \le i \le n} |y_i(t)|$$

L<sub>2</sub> (total energy) norm:

$$\|y\|_{2} = \left(\int_{0}^{\infty} y(t)^{T} y(t) dt\right)^{1/2}$$
$$= \left(\frac{1}{2\pi} \int_{-\infty}^{\infty} \hat{y}(j\omega)^{*} \hat{y}(j\omega) d\omega\right)^{1/2} \quad \text{(Parseval)}$$

root-mean-square seminorm:

$$\|y\|_{\mathsf{rms}} = \left(\lim_{T \to \infty} \frac{1}{T} \int_0^T y(t)^T y(t) \, dt\right)^{1/2}$$

#### **Common system norms**

Let *H* be a system with impulse response matrix h(t)

H<sub>2</sub> (RMS response to white noise):

$$|H||_{2} = \left(\operatorname{Tr} \frac{1}{2\pi} \int_{0}^{\infty} H(j\omega)^{*} H(j\omega) \, d\omega\right)^{1/2}$$
$$= \left(\frac{1}{2\pi} \sum_{i=1}^{n} \int_{-\infty}^{\infty} \sigma_{i} (H(j\omega))^{2} \, d\omega\right)^{1/2}$$
$$= \left(\operatorname{Tr} \int_{0}^{\infty} h(t)^{T} h(t) \, dt\right)^{1/2}$$

 $\textbf{H}_{\infty}$  (RMS or  $\textbf{L}_2$  gain):

$$\|H\|_{\infty} = \sup_{\|w\|_{2} \neq 0} \frac{\|Hw\|_{2}}{\|w\|_{2}} = \sup_{\omega} \sigma_{\max}(H(j\omega))$$

## Computing H<sub>2</sub>-norm

Consider the system

$$H: \dot{x} = Ax + B_w w, \quad z = C_z x, \quad x(0) = 0.$$

• impulse response is  $h(t) = C_z e^{At} B_w$ , follows from  $w(t) = \delta(t)$  in

$$y(t) = C_z \int_{0^-}^t e^{A(t-\tau)} B_w w(\tau) d\tau.$$

• substitute impulse response into

$$|H||_{2}^{2} = \operatorname{Tr}\left(\int_{0}^{\infty} h(t)^{T} h(t) dt\right)$$
$$= \operatorname{Tr}\left(B_{w}^{T} \int_{0}^{\infty} e^{A^{T} t} C_{z}^{T} C_{z} e^{At} dt B_{w}\right)$$
$$= \operatorname{Tr}(B_{w}^{T} W_{\text{obs}} B_{w})$$

## Computing H<sub>2</sub>-norm

The  $\mathbf{H}_2$  norm of the system satisfies

$$\|H\|_2^2 = \operatorname{Tr}(B_w^T W_{\operatorname{obs}} B_w),$$

where  $W_{\rm obs}$  is the observability Gramian, given by

$$W_{\rm obs} \stackrel{\Delta}{=} \int_0^\infty e^{A^{\mathsf{T}}t} C_z^{\mathsf{T}} C_z e^{At} dt,$$

or equivalently, the solution to the Lyapunov equation

$$A^T W_{\rm obs} + W_{\rm obs} A + C_z^T C_z = 0.$$

## **Controllability perspective**

Using the cyclic property of  $\mathbf{Tr}(\cdot)$ ,

$$\|H\|_{2}^{2} = \operatorname{Tr}\left(\int_{0}^{\infty} h(t)^{T} h(t) dt\right)$$
$$= \operatorname{Tr}\left(\int_{0}^{\infty} B_{w}^{T} e^{A^{T} t} C_{z}^{T} C_{z} e^{A t} B_{w} dt\right)$$
$$= \operatorname{Tr}\left(C_{z} \int_{0}^{\infty} e^{A t} B_{w} B_{w}^{T} e^{A^{T} t} dt C_{z}^{T}\right)$$
$$= \operatorname{Tr}(C_{z} W_{\text{contr}} C_{z}^{T}),$$

where  $W_{\rm contr}$  is the controllability Gramian,

$$W_{\rm contr} \triangleq \int_0^\infty e^{A^{\rm T}t} B_w B_w^{\rm T} e^{At} dt,$$

or equivalently, the solution to the Lyapunov equation

$$W_{\text{contr}}A^T + AW_{\text{contr}} + B_w B_w^T = 0.$$

## Lagrange duality

In fact, the following two SDPs are Lagrange duals of each other,

minimize 
$$\operatorname{Tr}(C_z Q C_z^T)$$
  
subject to  $Q \succeq 0,$  (1)  
 $Q A^T + A Q + B_w B_w^T \preceq 0$ 

and

maximize 
$$\mathbf{Tr}(B_w^T P B_w)$$
  
subject to  $P \succeq 0$   
 $A^T P + P A + C_z^T C_z \succeq 0$  (2)

• if strong duality obtains, then

$$\mathbf{Tr}(C_z Q^* C_z^T) = \mathbf{Tr}(B_w^T P^* B_w)$$

• strong duality is implied by strict feasibility of (1) or (2) ... which happens if A is stable.

## Strong duality in H<sub>2</sub> SDP

**link to H**<sub>2</sub> **norm.** If strong duality obtains in (1) and (2), and either  $P^* \succ 0$  or  $Q^* \succ 0$ , then

$$\|H\|_2^2 = \operatorname{Tr}(C_z Q^* C_z^T) = \operatorname{Tr}(B_w^T P^* B_w).$$

proof. by strong duality, we have

$$\begin{aligned} \mathbf{Tr}(C_z Q^* C_z^T) &= \mathbf{Tr}(B_w^T P^* B_w) \\ &= \inf_{Q \succeq 0} \mathbf{Tr}(C_z Q C_z^T) + \mathbf{Tr}((Q A^T + A Q + B_w B_w^T) P^*) \\ &\leq \mathbf{Tr}(C_z Q^* C_z^T) + \mathbf{Tr}((Q^* A^T + A Q^* + B_w B_w^T) P^*) \\ &\leq \mathbf{Tr}(C_z Q^* C_z^T), \end{aligned}$$

thus all the inequalities hold with equality. If  $P^{\star} \succ 0$ , then

$$Q^{\star}A^{T} + AQ^{\star} + B_{w}B_{w}^{T} = 0,$$

i.e.,  $Q^{\star} = W_{\text{contr.}}$  (If  $Q^{\star} \succ 0$  instead, we get  $P^{\star} = W_{\text{obs.}}$ )

## Strong duality in H<sub>2</sub> SDP

**fact.** If A is (Hurwitz) stable, then strong duality obtains in (1) and (2).

**proof.** if A is Hurwitz stable, there exists a matrix  $Q_0 \succ 0$  such that

$$Q_0A^T + AQ_0 + (\epsilon I + B_w B_w^T) = 0,$$

where  $\epsilon > 0$  is any positive number. Therefore

$$Q_0 A^T + A Q_0 + B_w B_w^T = -\epsilon I \prec 0,$$

meaning (1) is strictly feasible. By Slater's condition, we have strong duality.

## Strong duality in H<sub>2</sub> SDP

fact. Suppose A is (Hurwitz) stable.

- if  $(A, B_w)$  is controllable, then  $Q^* \succ 0$  and  $P^* = W_{obs}$
- if  $(A, C_z)$  is observable, then  $P^* \succ 0$  and  $Q^* = W_{contr}$

**proof (first statement).** since  $Q^*$  is feasible in (1), it is a generalized controllability Gramian, so it satisfies

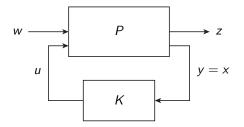
$$Q^{\star} \succeq W_{\text{contr}},$$

and because  $(A, B_w)$  is controllable with A Hurwitz, we further have  $W_{\text{contr}} \succ 0$ . Therefore  $Q^* \succeq W_{\text{contr}} \succ 0$ . From strong duality,

$$\mathbf{Tr}((A^T P^* + P^* A + C_z^T C_z)Q^*) = 0$$

implies  $A^T P^* + P^* A + C_z^T C_z = 0$ , thus,  $P^* = W_{obs}$ , as required.

## H<sub>2</sub> state feedback synthesis problem



Given the system

$$\dot{x} = Ax + B_u u + B_w w$$
,  $z = C_z x + D_{zu} u$ ,  $x(0) = 0$ 

find a state feedback input u = Kx to minimize the *w*-to-*z*  $H_2$  norm.

#### Interpretation: calculating the w-to-z H<sub>2</sub> norm

For constant state-feedback u = Kx, the closed loop system is

$$\dot{x} = (A + B_u K)x + B_w w$$
  
 $z = (C_z + D_{zu} K)x$ 

thus the w-to- $z \ \mathbf{H}_2$  norm is simply the energy of the output

$$E=\int_0^\infty z(t)^T z(t)\,dt,$$

with the choice  $w(t) = \delta(t)$ 

#### Calculating the *w*-to-z H<sub>2</sub> norm

Choosing  $w(t) = \delta(t)$  for the system

$$\dot{x} = (A + B_u K)x + B_w w$$
$$z = (C_z + D_{zu} K)x$$
$$x(0) = 0$$

is the same as having a nonzero initial condition  $x(0) = B_w$ 

$$\dot{x} = (A + B_u K)x$$
$$z = (C_z + D_{zu} K)x$$
$$x(0) = B_w,$$

proof.

$$\begin{aligned} x(t) &= e^{(A+B_uK)t} \cdot 0 + \int_{0^-}^t e^{(A+B_uK)(t-\tau)} B_w \cdot \delta(\tau) \, d\tau \\ &= e^{(A+B_uK)t} \cdot B_w \end{aligned}$$

## H<sub>2</sub> state feedback synthesis

In the language of the LMI (1), the w-to-z  $\mathbf{H}_2$  norm is given by solving the problem

minimize 
$$\operatorname{Tr} \left( (C_z + D_{zu}K)Q(C_z + D_{zu}K)^T \right)$$
  
subject to  $Q \succeq 0$   
 $Q(A + B_uK)^T + (A + B_uK)Q + B_wB_w^T \preceq 0$ 

- the objective is simulatenously the  $H_2$  norm, and the output energy E we wish to minimize.
- if  $A + B_u K$  is stable, strong duality obtains
- if K is a variable, the problem is nonconvex

### Lyapunov function perspective

output energy minimization

$$\dot{x} = Ax + B_u u, \quad z = C_z x + D_{zu} u \tag{3}$$

where (A, B, C) is minimal,  $D_{zu}^T D_{zu} \succ 0$ , and  $D_{zu}^T C_z = 0$ . Given an initial condition x(0) find an input u = Kx to minimize the output energy

$$E=\int_0^\infty z(t)^T z(t)\,dt.$$

**fact.** if there exists a storage function  $V(x) = x^T P x$ ,  $P \succ 0$ , and

$$rac{d}{dt}V(x)\leq -z^{T}z,$$
 for all  $z, x, u = Kx$  satisfying (3),

then  $x(0)^T P x(0)$  is an upper bound on E.

## Lyapunov argument

Integrate 
$$\frac{d}{dt}V(x) \leq -z^T z$$
 to get  
 $V(x(T)) - V(x(0)) \leq -\int_0^T z^T z \, dt$ , for all  $T \geq 0$ .

Since  $V(x(T)) \ge 0$ , and this is true for all T, we therefore have

$$V(x(0)) \geq \int_0^\infty z^T z \, dt \quad (=E).$$

•  $V(x(0)) = x(0)^T P x(0)$  is an upper bound on the output energy

· to make output energy small, we minimize this upper bound

#### Solution to problem

We wish to minimize the upper bound  $x(0)^T Px(0)$  subject to the dissipation condition:

$$\frac{d}{dt}V(x) \leq -z^{T}z$$
, for all  $z, x, u = Kx$  satisfying (3)

$$\Leftrightarrow \dot{x}^{T}Px + x^{T}P\dot{x} \leq -z^{T}z, \text{ for all } z, x, u = Kx \text{ satisfying (3)}$$

$$\Leftrightarrow x^{T}(A + B_{u}K)^{T}Px + x^{T}P(A + B_{u}K)x$$

$$\leq -x^{T}(C_{z} + D_{zu}K)^{T}(C_{z} + D_{zu}K)x, \text{ for all } x \in \mathbf{R}^{n}$$

$$\Leftrightarrow A^{T}P + PA + K^{T}B_{u}^{T}P + PB_{u}K + C_{z}^{T}C_{z} + K^{T}(D_{zu}^{T}D_{zu})K \leq 0$$

$$\Leftrightarrow QA^{T} + AQ + QK^{T}B_{u}^{T} + B_{u}KQ$$

$$+ (C_{z}Q)^{T}(C_{z}Q) + QK^{T}(D_{zu}^{T}D_{zu})KQ \leq 0$$

where in the last step we multiplied on the left and right by  $Q = P^{-1}$ 

#### State feedback trick

If we define the variable Y = KQ, then we have  $QA^T + AQ + QK^TB_u^T + B_uKQ + (C_zQ)^T(C_zQ) + QK^T(D_{zu}^TD_{zu})KQ \leq 0$   $\iff$  $QA^T + AQ + Y^TB_u^T + B_uY^T + (C_zQ)^T(C_zQ) + Y^T(D_{zu}^TD_{zu})Y \leq 0$ 

Taking a Schur complement gives the LMI

$$\begin{bmatrix} QA^{T} + AQ + Y^{T}B_{u}^{T} + B_{u}Y^{T} & (C_{z}Q + D_{zu}Y)^{T} \\ (C_{z}Q + D_{zu}Y) & -I \end{bmatrix} \leq 0$$

## Output energy minimization summary

#### state feedback synthesis. solve the problem

minimize 
$$\begin{aligned} & x(0)^T Q^{-1} x(0) \\ & \text{subject to} \quad \begin{bmatrix} QA^T + AQ + Y^T B_u^T + B_u Y^T & (C_z Q + D_{zu} Y)^T \\ & (C_z Q + D_{zu} Y) & -I \end{bmatrix} \leq 0, \\ & Q \succ 0 \end{aligned}$$

with variables  $Q = Q^T \in \mathbf{R}^{n \times n}$  and  $Y \in \mathbf{R}^{n_u \times n}$ 

#### solution.

• the optimal value  $x(0)^T (Q^*)^{-1} x(0)$  is an upper bound on the energy

$$E = \int_0^\infty z^{\mathsf{T}} z \, dt$$

• the optimal state feedback is  $K = Y^*(Q^*)^{-1}$ 

#### Bound on $H_\infty\text{-norm}$

Consider the system

$$H: \quad \dot{x} = Ax + B_w w, \quad z = C_z x, \quad x(0) = 0. \tag{4}$$

If there exists a storage function  $V: \mathbf{R}^n \to \mathbf{R}_+$  such that

$$\dot{V} + z^T z - \gamma w^T w \leq 0, \quad V(0) = 0$$

for all x and w satisfying (4), then  $||H||_{\infty}^2 \leq \gamma$ .

proof. integrate to obtain

$$\underbrace{\underbrace{\int_0^\infty \dot{V}(x(t)) dt}_{\geq 0} + \|z\|_2^2 \leq \gamma \|w\|_2^2}_{\geq 0}.$$

#### **Quadratic storage function**

For  $V(x) = x^T P x$ ,  $P \succ 0$ , the condition

$$\dot{V} + z^T z - \gamma w^T w \le 0$$

for all x and w satisfying (4), is the same as

$$(Ax + B_w w)^T P x + x^T P (Ax + B_w w) + x^T (C_z^T C_z) x - \gamma w^T w \leq 0.$$

This translates to the LMI:

$$P \succ 0, \quad \begin{bmatrix} A^T P + PA + C_z^T C_z & PB_w \\ B_w^T P & -\gamma I \end{bmatrix} \preceq 0.$$

## Calculating the $H_\infty\text{-norm}$ of a system

Now consider minimizing the upper bound  $\gamma$ ,

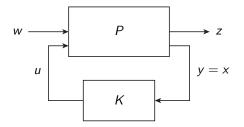
$$\begin{array}{ll} \text{minimize} & \gamma \\ \text{subject to} & P \succ 0 \\ & \begin{bmatrix} A^T P + PA + C_z^T C_z & PB_w \\ & B_w^T P & -\gamma I \end{bmatrix} \preceq 0. \end{array}$$

**fact.** (Kalman–Yakubovich–Popov) the optimal solution to the problem above is  $\gamma^* = \|H\|_{\infty}^2 = \|C_z(sI - A)^{-1}B_w\|_{\infty}^2$ .

- quadratic storage function is enough
- worst case gain is the  $H_{\infty}$ -norm (suitably squared):

$$\|z\|_{2}^{2} \leq \gamma \|w\|_{2}^{2} \iff \|H\|_{\infty}^{2} = \sup_{\|w\|_{2} \neq 0} \frac{\|z\|_{2}^{2}}{\|w\|_{2}^{2}} \leq \gamma$$

## $H_\infty$ state feedback synthesis problem



Given the system

$$\dot{x} = Ax + B_u u + B_w w$$
,  $z = C_z x + D_{zu} u$ ,  $x(0) = 0$ 

find a state feedback input u = Kx to minimize the *w*-to-*z*  $\mathbf{H}_{\infty}$  norm.

#### $H_\infty$ state feedback solution

Once again, we minimize the  $\boldsymbol{H}_\infty$  norm upper bound for the closed loop system

$$\dot{x} = (A + B_u K)x + B_w w$$
$$z = (C_z + D_{zu} K)x$$
$$x(0) = 0,$$

*i.e.*, we wish to solve the nonconvex problem

$$\begin{array}{ll} \text{minimize} & \gamma \\ \text{subject to} & P \succ 0 \\ \begin{bmatrix} (A + B_u K)^T P + P(A + B_u K) + (C_z + D_{zu} K)^T (C_z + D_{zu} K) & PB_w \\ & B_w^T P & -\gamma I \end{bmatrix} \leq 0. \end{array}$$

## $H_\infty$ state feedback synthesis solution

A sequence of manipulations with Y = KQ gives the equivalent problem

$$\begin{array}{ll} \text{minimize} & \gamma \\ \text{subject to} & Q \succ 0 \\ \begin{bmatrix} AQ + QA^T + B_uY + Y^TB_u^T + B_wB_w^T & (C_zQ + D_{zu}Y)^T \\ C_zQ + D_{zu}Y & -\gamma I \end{bmatrix} \preceq 0. \end{array}$$

• optimal controller is 
$$K = Y^*(Q^*)^{-1}$$

#### Time domain properties

Let's explore the input to state properties of the LDI

$$\dot{x} = A(t)x + B_w(t)w, \quad [A(t) \quad B_w(t)] \in \Omega.$$
 (5)

Consider the following subsets of  $\mathbf{R}^n$ :

• reachable set with unit-energy input:

$$\mathcal{R}_{ue} = \left\{ x(T) \in \mathbf{R}^n \, \middle| \begin{array}{c} x, w \text{ satisfy (5)}, \quad x(0) = 0, \\ \int_0^T w^T w \, dt \le 1, \quad T \ge 0 \end{array} \right\}$$

• reachable set with unit-peak input:

$$\mathcal{R}_{up} = \begin{cases} x(T) \in \mathbf{R}^n & x, w \text{ satisfy } (5), \quad x(0) = 0, \\ w^T w \le 1, \quad T \ge 0 \end{cases}$$

• ellipsoid parameterized by P:

$$\mathcal{E} = \{ x \in \mathbf{R}^n \mid x^T P x \le 1 \}$$

### Bounding $\mathcal{R}_{ue}$ with an ellipsoid

The following inclusion holds:

• 
$$\mathcal{R}_{ue} \subseteq \mathcal{E}$$
 if there exists  $V(x) = x^T P x$ ,  $P \succ 0$ , such that

 $\dot{V}(x) \leq w^T w$ , for all x, w satisfying (5).

**proof.** suppose such V exists and  $x(T) \in \mathcal{R}_{ue}$ , where (recall)

$$\mathcal{R}_{ue} = \left\{ x(T) \in \mathbf{R}^n \, \middle| \begin{array}{c} x, w \text{ satisfy } (5), \quad x(0) = 0, \\ \int_0^T w^T w \, dt \le 1, \quad T \ge 0 \end{array} \right\}.$$

For this landing state x(T) and any input w that gets us there,

$$V(x(T)) - V(x(0)) = \int_0^T \dot{V}(x(t)) dt \le \int_0^T w^T w dt \le 1$$

therefore  $x(T)^T Px(T) \leq 1$ , *i.e.*,  $x(T) \in \mathcal{E}$ 

## Bounding $\mathcal{R}_{up}$ with an ellipsoid

The following inclusion holds:

•  $\mathcal{R}_{up} \subseteq \mathcal{E}$  if there exists  $V(x) = x^T P x$ ,  $P \succ 0$ , such that

 $\dot{V}(x) \leq 0$ , for all x, w satisfying (5),  $w^T w \leq 1$ , and  $V(x) \geq 1$ .

**proof idea.** for any admissible input (satisfying pointwise unit peak constraints  $w^T w \le 1$ ), as soon as  $V(x(T)) \ge 1$  at some time T, then for all times t thereafter,

$$V(x(t)) \leq V(x(T))$$
, for all  $t \geq T$ .

In other words, trajectories with an admissible input cannot exit the 1-sublevel set  $\{x \mid V(x) \leq 1\}$ .

#### Ellipsoidal bounds on reachable sets

For LTI systems  $\Omega = [A, B]$ , the reachability conditions can be rewritten

•  $\mathcal{R}_{ue} \subseteq \mathcal{E}$ : there exists  $V(x) = x^T P x$ ,  $P \succ 0$ , such that

 $\dot{V}(x) \leq w^T w$ , for all x, w satisfying (5).

is equivalent to feasibility of

$$P \succ 0, \quad \begin{bmatrix} A^T P + P A & P B_w \\ B_w^T P & -I \end{bmatrix} \preceq 0.$$

•  $\mathcal{R}_{up} \subseteq \mathcal{E}$ : there exists  $V(x) = x^T P x$ ,  $P \succ 0$ , such that

 $\dot{V}(x) \leq 0$ , for all x, w satisfying (5),  $w^T w \leq 1$ , and  $V(x) \geq 1$ .

is implied by feasibility of the bilinear matrix inequality

$$P \succ 0, \quad \alpha \ge 0, \quad \begin{bmatrix} A^T P + PA + \alpha P & PB_w \\ B_w^T P & -\alpha I \end{bmatrix} \preceq 0.$$